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20. M219 CAVITY CASE

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INTRODUCTION

The data contained in this set consists of pressure time histories measured on the ceiling of an empty rectangular cavity, and were measured as part of a joint BAe./DERA programme at the ARA wind tunnel at Bedford during November 1991. The overall programme consisted of several configurations, with bodies positioned at various proximities to the cavity, but the data presented here only considers the empty cavity, configured for both shallow and deep cases. Data were measured using Kulite transducers along the centreline of the rig, (which did not coincide with the centreline of the cavity itself), and, in an alternative configuration, on the centreline of the cavity. Measurements taken off the cavity centreline, but not included here, indicated that 3D effects were not significant.

DEFINITIONS

d Depth of Cavity

L Length of Cavity (20 in.)

M Mach Number P Pressure (KPa)

X, Y, Z Co-ordinate directions: X is in direction of the

flow. Y is span-wise and Z the vertical directions.

Note that all lengths are given in feet or inches except for boundary layer and transition lengths which are given in mm.

FORMULARY

1 GENERAL DESCRIPTION OF MODEL

1.1 Designation Model M219 (referred to as 'generic cavity rig')
 1.2 Type Empty Cavity (shallow and deep configurations).

1.3 Derivation DERA model manufactured at ARA

1.4 Additional remarks

The data are for 3D cavity. However, further data is available which suggests that there is no variation across

the inner 50% of cavity width.

1.5 References

2 MODEL GEOMETRY

2.1 Plan-form Rectangular cavity 20 in. X 4 in. (length X width). Two

depths: 2 in. and 4 in.

2.2 Rig geometry Flat surface model with inset cavity (see fig 1)

2.3 Cavity position in rig Cavity offset by 1 in. from flat surface centreline (see fig

1). Cavity leading edge 31 in. aft of flat plate leading

edge.

2.4 Additional remarks Full geometry in attached figures.

2.5 References 1,2

3 WIND TUNNEL

3.1 Designation ARA TWT (Transonic Wind Tunnel)

3.2 Type of tunnel Continuous flow
3.3 Test section dimensions 9 X 8 (ft.)

5.14 References

Ventilated 3.4 Type of roof and floor Ventilated 3.5 Type of side walls Perforated steel plate, 22% open area 3.6 Ventilation geometry Typically 13 mm at model centre-of-rotation station, 3.7 Thickness of side wall boundary layer (empty tunnel with centreline probe). Typically 13 mm at model centre-of-rotation station, 3.8 Thickness of boundary layers at roof and floor (empty tunnel with centreline probe). Settling chamber and working section static pressures with 3.9 Method of measuring Mach number calibrated corrections. <0.2° 3.10 Flow angularity <\$\preceq\$0.0005, (low subsonic, fan only), to <\$\preceq\$0.01, (high 3.11 Uniformity of Mach number over test section supersonic, nozzle setting plus plenum suction). Noise: Broadband rms. CP < 0.5% across Mach range. 3.12 Sources and levels of noise in empty tunnel Turbulence, (subsonic): u'/U<0.1%, v'/U<0.2% Fan blade passing frequency and harmonics. 3.13 Tunnel resonance's None 3.14 Additional remarks 3, 4 3.15 References on tunnel MODEL MOTION 4.1 General description No motion. On-line monitoring of accelerometers indicated no significant model motion. Output from datum pressure transducers, positioned on the flat plate (K1 and K2, see table 1), is available, although not included in this report. This indicated that there were no significant model or tunnel contributions to the unsteady cavity data. zero 4.2 Angle of attack **TEST CONDITIONS** 5.1 Model plan-form area/tunnel area 11.81% 15.74%, (17in/9ft) 5.2 Model span/tunnel width 1.16% (119.91 in²) 5.3 Blockage Rig support sting centreline 6in above tunnel centreline at 5.4 Position of model in tunnel zero incidence. 0.6, 0.85, 1.35 5.5 Range of Mach numbers 1.0032 to1.0121 bar 5.6 Range of tunnel total pressure 5.7 Range of tunnel total temperature 302.32 to 311.35 deg. K 5.8 Range of model steady, or mean incidence Zero incidence only. 5.9 Definition of model incidence 5.10 Position and type of transition trip 40 mm aft of leading edge of flat plate. Stream-wise width of strip 4 mm. Sparsely distributed ballotini 0.13 to 0.15 mm diameter. None 5.11 Flow instabilities during tests Not measured, very stiff model 5.12 Changes to mean shape of model due to steady aerodynamic load 5.13 Additional remarks None

1,2

MEASUREMENTS AND 6 **OBSERVATIONS**

6.1 Steady pressures for the mean conditions No 6.2 Steady pressures for small changes from the No mean conditions

6.3 Quasi-steady pressures Yes (for all conditions, but data not included in this

report).

No

No

Yes 6.4 Unsteady pressures 6.5 Steady section forces for the mean conditions by No integration of pressures

6.6 Steady section forces for small changes from the mean conditions by integration

6.7 Quasi-steady section forces by integration No 6.8 Unsteady section forces by integration No

6.9 Measurement of actual motion at points on No

6.10 Observation of measurement of boundary-layer properties

6.11 Visualisation of surface flow No 6.12 Visualisation of shock wave movements No 6.13 Additional remarks None

INSTRUMENTATION

7.1 Steady/Quasi steady pressures

7.1.1 Position of orifices span-wise and chord-

Front plate, rear plate, cavity ceiling, cavity sidewalls, cavity front wall. For distribution see attached figures and table 2.

7.1.2 Type of measuring system

Pressure orifices in model surfaces. Pressure measurement by PSI electronic scanning modules.

7.2 Unsteady pressures

7.2.1 Position of orifices span-wise and chord-

2 on flat plate ahead of cavity, 2 on front wall of cavity, 10 positioned along ceiling of cavity either on its centreline, (shallow cavity), or 1 inch offset, (deep cavity; note this is the centreline of the rig), and 1 on flat plate aft of cavity.

(See figure 1 and table 2)

7.2.2 Diameter of orifices 0.09in diameter transducers behind 0.063in diameter

orifices.

7.2.3 Type of measuring system High speed digital data acquisition system. Data sampled

7.2.4 Type of transducers Kulite miniature high response XCO 25PSI differential.

7.2.5 Principle and accuracy of calibration Calibrated in situ by application of range of steady

pressures

7.3 Model motion

7.3.1 Method of measuring motion reference co-ordinate

7.3.2 Method of determining spatial mode of motion

7.3.3 Accuracy of measured motions

N/A

N/A

N/A

7.4 Processing of unsteady measurements

7.4.1 Method of acquiring and processing

measurements

7.4.2 Type of analysis

High speed digital data acquisition system. Data sampled at $6000\ Hz$

Spectral analysis using FFT to obtain power spectral density, rms. amplitude versus frequency and rms. total sound pressure level. Block size 2048 and summation of moving averages.

7.4.3 Unsteady pressure quantities obtained and accuracies achieved

Time history data. Spectral data

7.4.4 Method of integration to obtain forces

7.5 Additional remarks

7.6 References on techniques

Standard "Text Book" techniques have been used.

8 DATA PRESENTATION

8.1 Test cases for which data could be made available

M=0.4, 0.80, 0.98, 1.10 and 1.19.

8.2 Test cases for which data are included in this document

uns

8.3 Steady pressures

8.4 Quasi-steady or steady perturbation pressures

N/A No

N/A

None

8.5 Unsteady pressures

Pressure time history for each pressure tap on cavity

Two configurations (shallow and deep) each at M=0.6,

ceiling.

0.85, 1.35

RMS pressure for each pressure tap on cavity ceiling.

8.6 Steady forces or moments

8.7 Quasi-steady or steady perturbation forces N/A

8.8 Unsteady forces and moments

N/A

N/A

8.9 Other forms in which data could be made available

Spectral data in rms. amplitude versus frequency form or power spectral density. It is recommended that the reader carry out signal analysis of the experimental data with the same tools that will be used to analyse the CFD data.

8.10 References giving other presentation of data

The data for empty cavity geometries has not been discussed in the open literature. Other reports on related work with non-empty cavities may be made available through application to DERA.

9 COMMENTS ON DATA

9.1 Accuracy

 9.1.1 Mach number
 ±0.001

 9.1.2 Steady incidence
 ±0.01deg

9.1.3 Steady pressure coefficients

Basic accuracy of system in measuring a steady pressure coefficient at total pressures around atmospheric has been shown to be $\pm 0.5\%$. However, for the current data steady or quasi-steady pressure coefficients are essentially a time average of a varying pressure and will be less accurate. Quasi-steady pressure coefficients measured at different times have been shown to be repeatable to within $\pm 3\%$.

9.1.4 Steady pressure derivatives

N/A

9.1.5 Unsteady pressure coefficients

Combined non-linearity and hysteresis of Kulite transducers 0.1% of full-scale output; refer to DERA calibration of entire measurement chain.

9.2 Sensitivity to small changes of parameter

The only parameter varied was Mach number; changes other than those listed were not investigated.

- 9.3 Non-linearities
- 9.4 Influence of tunnel total pressure
- 9.5 Effects on data of uncertainty, or variation, in mode of model motion
- 9.6 Wall interference corrections
- 9.7 Other relevant tests on same model
- 9.8 Relevant tests on other models of nominally the same shape
- 9.9 Any remarks relevant to comparison between experiment and theory
- 9.10 Additional remarks
- 9.11 References on discussion of data

10 PERSONAL CONTACT FOR FURTHER INFORMATION

11 LIST OF REFERENCES

N/A

Tunnel total pressure remained nominally constant at 1 har

N/A

Corrections have been made to Mach number for tunnel blockage due to presence of the model and support system. Other tests have been made on the same model with stores mounted within the cavity.

N/A

Methods, under development, for the computation of cavity flow fields gave reasonable agreement between experiment and theory for time averaged or quasi-steady pressures. Early computations of rms. unsteady pressure levels using 2-D methods significantly over-predicted levels in comparison with the measured values.

None

The data for empty cavity geometries has not been discussed in open literature. Other reports on related work with non-empty cavities may be made available through application to DERA.

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- Aircraft Research Association Ltd., Model Test Note M219/6 "Details of tests in the ARA 2.74m x 2.44m transonic wind tunnel measuring the release disturbance of weapons carried in cavities." Feb 1993.
- Aircraft Research Association Ltd. Model Test Note M157/5 "Feasibility study for the measurement of release disturbance of weapons carried in cavities. April 1989.
- Green J. E., McHugh C.A., Baxendale A.J. and Stanniland D. R., 'The use of a deep honeycomb to achieve high flow quality in the ARA 9' x 8' Transonic Wind Tunnel', presented at 18th Congress of ICAS, Beijing, September 1992.
- Stanniland D. R., McHugh C.A. and Green J.E., 'Improvement of the flow quality in the ARA Transonic Tunnel by means of a long cell honeycomb', paper 54, RAeS conference on "Wind Tunnels and Wind Tunnel Test Techniques", Southampton, 1992.

EXPERIMENTAL ARRANGEMENT

The test rig dimensions are given in figure 1, the spoiler was not in place for the tests reported herein and is noted for information only. The location of the kulite transducers for which data is recorded in this database are shown in table 1 and illustrated in Figure 2. for the deep cavity. The cavity centreline is displaced by 1" relative to the rig centreline (see figure 1). For the deep (4") cavity the kulites are positioned on the rig centreline (Y=0), which is 1" to port of cavity centreline. For the shallow (2") cavity the kulites are positioned at Y=1.0 (equivalent to the cavity centreline).

There were also 28 static pressure measurement transducers ahead of the cavity (on the rig centreline) and 14 aft of the cavity. Static measurement locations inside the cavity are noted in table 2.

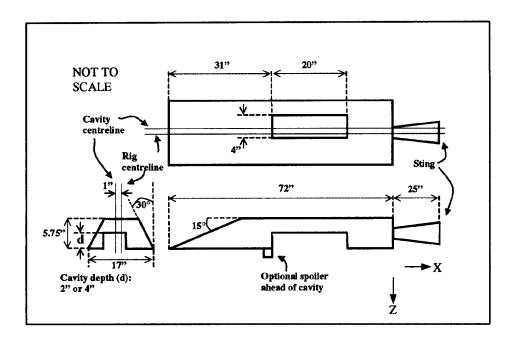


Figure 1: Test Rig and Dimensions

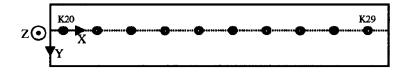


Figure 2: Position of Kulite Transducers on Cavity Ceiling (deep cavity)

-

¹ Cavity is on the rig underside.

DATA LAYOUT

The data is stored in six files (one for each flow condition), and consists of ten columns corresponding to the ten ceiling transducers in the order K20 to K29 (figure 2). Each column contains the pressure time history in KPa, with each row written in the FORTRAN format 10F14.6.

The time step for the data is implicit in the sampling rate per channel, i.e. a time step of $\frac{1}{6000}$ seconds.

Data files are located in the tree shown in figure 3.

Plots and values of the rms. pressure are included in table 3 (see figures 4 and 5) for the purpose of checking data quality. The values are derived including power up to 3000Hz, using the following parameters:

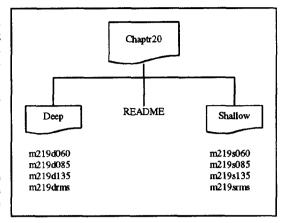


Figure 3: Layout of electronic data

Sampling frequency

6000

Block size

1024

(samples/second)
Block period (seconds)

0.17067

7 Number of averages

20

No windowing was used in this analysis.

| Kulite | X(in) | X/L | Location | Y(in) | |
|-------------|--------------|---------------|-------------|-------|---------|
| K1 | -7.0 | | Front | 0.0 | |
| K2 | -4.0 | İ | plate | 0.0 | |
| K4 | 39.9 | | Rear plate | -3.0 | |
| K7 | 0.0 | | Front wall | 2.5 | |
| K8 | 0.0 | | (Z=-1.0) | - | 0.5 |
| | | | 2" cavity | | |
| K 9 | 0.0 | | Front wall | 2.5 | |
| K 10 | 0.0 | | (Z=-1.0) | - | 0.5 |
| | | | 4" cavity | | _ |
| | | | | Deep | Shallow |
| K20 | 1.0 | 0.05 | | 0.0 | 1.0 |
| K21 | 3.0 | 0.15 | | 0.0 | 1.0 |
| K22 | 5.0 | 0.25 |] | 0.0 | 1.0 |
| K23 | 7.0 | 0.35 | | 0.0 | 1.0 |
| K24 | 9.0 | 0.45 | Cavity | 0.0 | 1.0 |
| K25 | 11.0 | 0.55 | œiling | 0.0 | 1.0 |
| K26 | 13.0 | 0.65 | | 0.0 | 1.0 |
| K27 | 15.0 | 0.75 | | 0.0 | 1.0 |
| K28 | 17.0 | 0.85 | | 0.0 | 1.0 |
| K29 | 19.0 | 0.95 | | 0.0 | 1.0 |
| K37 | Port wall wo | rking section | Tunnel wall | | |

Table 1 Locations of Kulite transducers, only measurements from those on the cavity ceiling are included in this database.

| | 2" Depth Cavity | 4"Depth Cavity |
|---------------------|------------------------|----------------------|
| Ceiling | 16 at Y=0", 16 at Y=2" | 16 at Y=2" |
| Front Wall | 8 at Y=2" | 8 at Y=0", 8 at Y=2" |
| Port Side Wall | 20 at Y=-1", Z=-0.25" | 20 at Y=1", Z=-0.25" |
| Starboard Side Wall | 20 at Y=3", Z=-0.25" | 20 at Y=3", Z=-0.25" |

Table 2 Static Pressure Measurements Inside Cavity

| X /L | Deep Cavity | | | Shallow Cavity | | |
|-------------|-------------|--------|--------|----------------|--------|--------|
| | M=0.6 | M=0.85 | M=1.35 | M=0.6 | M=0.85 | M=1.35 |
| 0.050 | 0.469 | 1.053 | 2.699 | 0.229 | 0.325 | 0.565 |
| 0.150 | 0.462 | 0.923 | 1.835 | 0.286 | 0.381 | 0.523 |
| 0.250 | 0.486 | 1.083 | 1.590 | 0.488 | 0.555 | 0.707 |
| 0.350 | 0.654 | 1.366 | 2.947 | 0.814 | 0.858 | 0.873 |
| 0.450 | 0.897 | 1.716 | 4.498 | 0.908 | 1.221 | 1.101 |
| 0.550 | 1.046 | 2.079 | 4.742 | 0.721 | 1.285 | 1.372 |
| 0.650 | 1.157 | 2.318 | 4.280 | 0.595 | 1.209 | 1.720 |
| 0.750 | 1.489 | 2.572 | 3.864 | 0.586 | 1.241 | 1.917 |
| 0.850 | 1.929 | 3.490 | 5.724 | 0.799 | 1.604 | 2.263 |
| 0.950 | 2.068 | 4.117 | 8.505 | 1.606 | 3.030 | 3.358 |

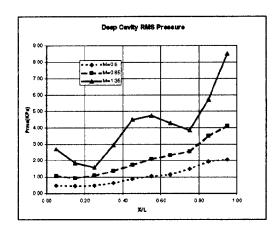


Figure 4: RMS Pressure distribution along the ceiling of the 'deep' empty cavity.

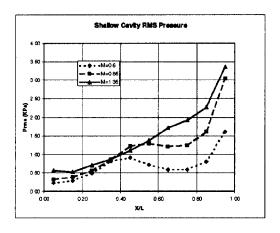


Figure 5: RMS Pressure distribution along the ceiling of the 'shallow' empty cavity.

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